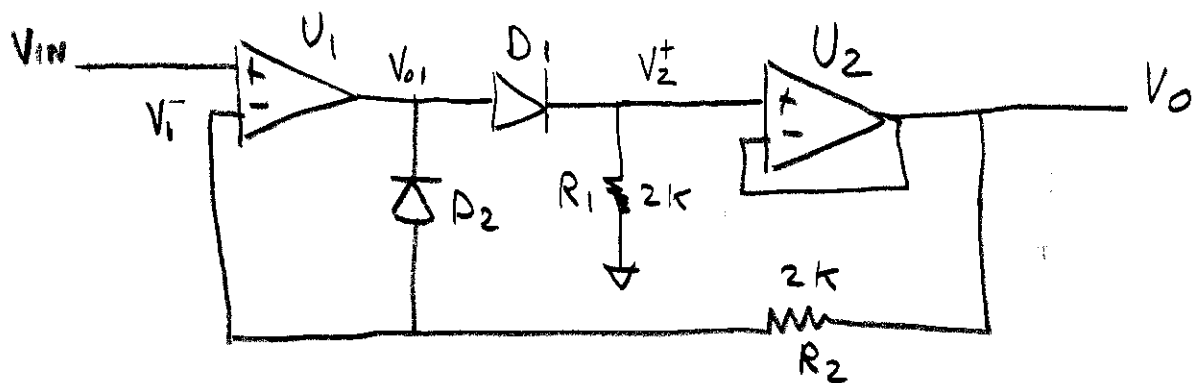


# DIODE CIRCUITS

## HALF WAVE RECTIFIER



ANALYSIS FOR  $V_{IN} > 0$ :

NOTE THAT  $V_2^+ = V_0$  SINCE  $U_2$  HAS GAIN OF 1

$$V_{01} = V_2^+ + V_{D1}$$

SINCE  $V_1^- = V_0$  BECAUSE  $D_2$  IS NOW REVERSE BIASED AND THERE IS NO CURRENT THROUGH  $R_2$ .

SO  $V_0 = V_{IN}$

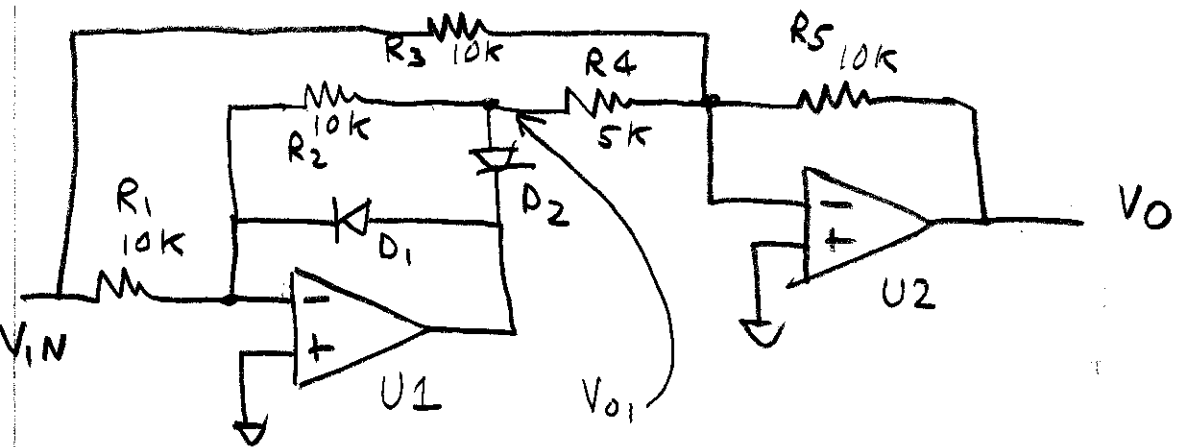
ANALYSIS FOR  $V_{IN} < 0$ :

NOW  $V_{01} = V_{IN} - V_{D2}$  SO  $V_1^- = V_{IN}$

$D_1$  IS REVERSE BIASED SO  $V_2^+ = 0$  AND  $V_0 = 0$

PURPOSE OF  $R_2$  IS TO PROVIDE FEEDBACK PATH WHEN  $V_{IN} > 0$  AND TO NOT BE TOO SMALL WHEN  $V_{IN} < 0$ . GENERALLY,  $R_1 + R_2$  ARE AS SMALL AS POSSIBLE TO MINIMIZE TIME CONSTANTS THAT DEGRADE PERFORMANCE AT HIGH FREQUENCIES.

# FULL WAVE RECTIFIER (ABSOLUTE VALUE CIRCUIT)



NOTE:  $V_{01} = -V_{IN}$  FOR  $V_{IN} > 0$   
 $V_{01} = 0$  FOR  $V_{IN} < 0$

$$V_0 = -V_{IN} \left( \frac{R_5}{R_3} \right) - V_{01} \left( \frac{R_5}{R_4} \right)$$

$$= -V_{IN} (1) - V_{01} (2)$$

$V_{IN} > 0$  ;  $V_0 = -V_{IN} - (-V_{IN})(2)$

$$\underline{\underline{V_0 = V_{IN}}}$$

$V_{IN} < 0$  ;  $V_0 = -V_{IN} - (0)(2)$

$$\underline{\underline{V_0 = -V_{IN}}}$$

