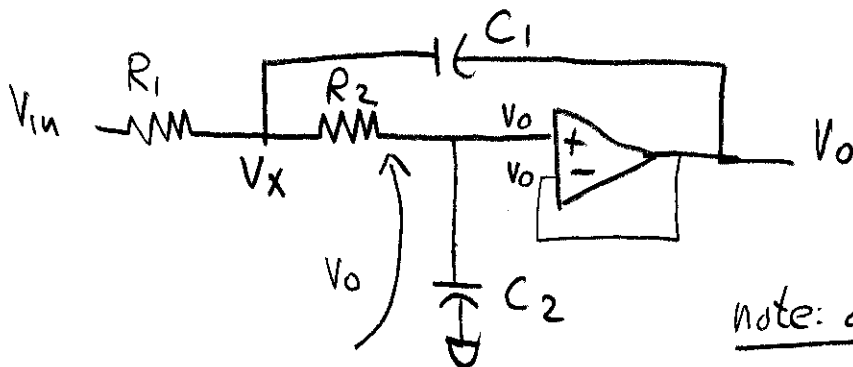


# SALLEN-KEY UNITY GAIN LOW-PASS FILTER

1 of 2



June 4, 1998

K. Kuhn

note: all V's are V'(s)

$$\frac{V_{in} - V_x}{R_1} = \frac{V_x - V_o}{R_2} + \frac{V_x - V_o}{1/C_1 s}$$

$$R_2(V_{in} - V_x) = R_1(V_x - V_o) + R_1 R_2 C_1 s (V_x - V_o)$$

$$V_o = \frac{V_x}{R_2 C_2 s + 1}$$

$$\therefore V_x = V_o (R_2 C_2 s + 1)$$

$$R_2(V_{in} - V_o(R_2 C_2 s + 1)) = R_1 V_o (R_2 C_2 s) + R_1 R_2 C_1 V_o (R_2 C_2 s)$$

$$V_o (R_1 C_2 s + R_1 C_1 R_2 C_2 s^2 + R_2 C_2 s + 1) = V_{in}$$

$$\frac{V_o(s)}{V_{in}(s)} = \frac{1}{R_1 C_1 R_2 C_2 s^2 + (R_1 + R_2) C_2 s + 1}$$

$$= \frac{1/R_1 C_1 R_2 C_2}{s^2 + \frac{R_1 + R_2}{R_1 R_2 C_1} s + \frac{1}{R_1 C_1 R_2 C_2}}$$

$$= \frac{\omega_n^2}{s^2 + 2 \zeta \omega_n s + \omega_n^2}$$

$$\omega_n = \frac{1}{\sqrt{R_1 R_2 C_1 C_2}}$$

$$z \zeta \omega_n = \frac{R_1 + R_2}{R_1 R_2 C_1}$$

$$\frac{z \zeta}{\sqrt{R_1 R_2 C_1 C_2}} = \frac{R_1 + R_2}{R_1 R_2 C_1}$$

$$\zeta = \left(\frac{1}{2}\right) \left(\frac{R_1 + R_2}{R_1 R_2 C_1}\right) \sqrt{R_1 R_2 C_1 C_2}$$

$$\zeta = \frac{(R_1 + R_2)}{2} \sqrt{\frac{C_2}{R_1 R_2 C_1}}$$

Analytic  
Equations

Analysis: Given  $R_1, R_2, C_1, C_2$  Find  $\omega_n, \zeta$   
 Design: Given  $\omega_n, \zeta$  Find  $R_1, R_2, C_1, C_2$

There are infinite design solutions possible but only a limited set is practical. Generally:

- \*  $R_1$  OR  $R_2$  should be greater than about 1k
- \*  $R_1$  OR  $R_2$  should be less than about 1Meg
- \*  $C_1$  OR  $C_2$  should be greater than about 300 pF
- \*  $C_1$  OR  $C_2$  should be less than about 1uF

There are a number of possible design solutions.

A good example of a practical approach is contained within the spreadsheet `sk-des.xls`. The student will have to derive the math which is rather complicated — typical of design math.

# SALLÉN-KEY LPF DESIGN

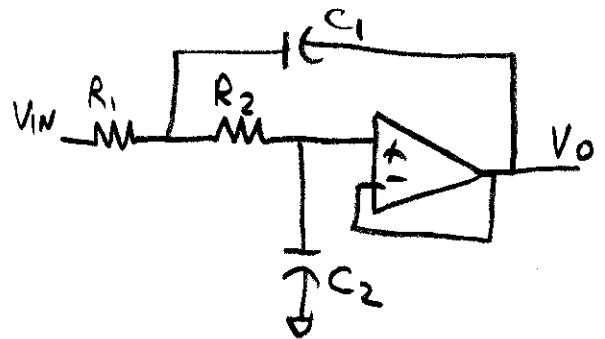
1/2

K. KUHN

FROM ANALYSIS:

$$\omega_n = \frac{1}{\sqrt{R_1 R_2 C_1 C_2}}$$

$$\zeta = \frac{R_1 + R_2}{2} \sqrt{\frac{C_2}{R_1 R_2 C_1}}$$



WE CAN WRITE:

$$\zeta^2 = \frac{(R_1 + R_2)^2}{4 R_1 R_2} \left( \frac{C_2}{C_1} \right) = \frac{R_1^2 + 2 R_1 R_2 + R_2^2}{4 R_1 R_2} \left( \frac{C_2}{C_1} \right)$$

$$= \left( \frac{R_1}{4 R_2} + \frac{1}{2} + \frac{R_2}{4 R_1} \right) \left( \frac{C_2}{C_1} \right)$$

$$= \left( \frac{1}{4 (R_2/R_1)} + \frac{1}{2} + \frac{(R_2/R_1)}{4} \right) \left( \frac{C_2}{C_1} \right)$$

$$\left( \frac{R_2}{R_1} \right) \zeta^2 = \left( \frac{1}{4} + \frac{R_2/R_1}{2} + \frac{(R_2/R_1)^2}{4} \right) \left( \frac{C_2}{C_1} \right)$$

$$\left( \frac{C_2/C_1}{4} \right) \left( \frac{R_2}{R_1} \right)^2 + \left( \frac{C_2/C_1}{2} - \zeta^2 \right) \left( \frac{R_2}{R_1} \right) + \frac{C_2/C_1}{4} = 0$$

$$\frac{R_2}{R_1} = \zeta^2 - \frac{C_2/C_1}{2} + \sqrt{\left( \frac{C_2/C_1}{2} - \zeta^2 \right)^2 - \frac{(C_2/C_1)^2}{4}}$$

$$\left( \frac{C_2/C_1}{4} \right)$$

$$\frac{R_2}{R_1} = \frac{2\omega^2 - \frac{C_2}{C_1} + 2\sqrt{\frac{(C_2/C_1)^2}{4} - 2\frac{(C_2/C_1)\omega^2 + \omega^4}{2}} - \frac{(C_2/C_1)^2}{4}}{(C_2/C_1)}$$

$$\frac{R_2}{R_1} = \frac{2\omega^2 - \left(\frac{C_2}{C_1}\right) + 2\omega\sqrt{\omega^2 - \left(\frac{C_2}{C_1}\right)}}{(C_2/C_1)}$$

NOTE:

$$\frac{C_2}{C_1} \leq \omega^2 \quad \text{for real sqrt}$$

PROCEDURE:

① DETERMINE  $C = \sqrt{C_1 C_2} = \frac{4 \times 10^{-7}}{\sqrt{\text{Frequency (Hz)}}}$  Farads

②  $C_1 = C/\omega$  and round  $C_1$  to near std value

③  $C_2 < \omega^2 C_1$  and round  $C_2$  down to convenient std value

④  $K = \frac{R_2}{R_1} = \frac{2\omega^2 - \left(\frac{C_2}{C_1}\right) + 2\omega\sqrt{\omega^2 - \frac{C_2}{C_1}}}{C_2/C_1}$

⑤  $R^2 = R_1 R_2 = \frac{1}{\omega^2 C_1 C_2}$

⑥  $K R_1^2 = R^2 \quad \therefore R_1 = \sqrt{\frac{R^2}{K}}$  round to closest std value

⑦  $R_2 = \frac{R^2}{R_1}$  round to closest std value